

Study of RBF Nerve Network Tuning PD Control Algorithm of Bilateral Servo System

Guang Wen
School of Machinery and Engineering, Pan-zhuhua University
Pan-zhuhua, 617000, China

Abstract

In construction tele-robot system. When p-f architecture force feedback was used, the impact of large feedback force result in the strike-like feeling on the operator's hand. If the amplitude is high, it will cause the control unstable. So a improved force feedback control method with the feature of a T-S fuzzy feedback coefficient, which could be modified online nonlinearly and continuously, is developed. A RBF-PID force controller is also designed, and formed a bilateral hydraulic servo control system. The experimental results indicate that the new improved control method reduced the impact of the feedback force, enhanced the compliance and transparency of the tele-operation of construction tele-robot system.

Keywords: Fuzzy feedback coefficient; Force Feedback; Construction Tele-robot

1. Introduction

Master, slave tele-operation robot system works can be inaccessible in the human person harmful to the environment or to complete work. Operators in a safe place that only a true and accurate force tele-presence information, they can control engineering task robot to accurately complete the operation. Pairs of force tele-presence tele-operation robot control system design projects, to ensure system stability, reliability, and tracking performance, So effective control methods, rational design of the controller is the critical to ensure the reliable operation of control systems[1~5]. Authors based on the existing control methods and their application in the field of robotics research, combined with force tele-presence tele-operation robot works bi-directional hydraulic servo control system characteristics, relying on electro-hydraulic proportional valve controlled by the master, from the hydraulic swing motor experimental platform consisting of tele-presence. Force feedback servo-control for bi-directional feedback exists in the impact force the issue, proposed to improve the force feedback control method to increase the smoothness. Experimental results show the effectiveness of the method[6].

This document is set in 10-point Times New Roman. If absolutely necessary, we suggest the use of condensed line spacing rather than smaller point sizes. Some technical formatting software print mathematical formulas in italic type, with subscripts and superscripts in a slightly smaller font size. This is acceptable.

2. Improved bi-directional force feedback servo-control method

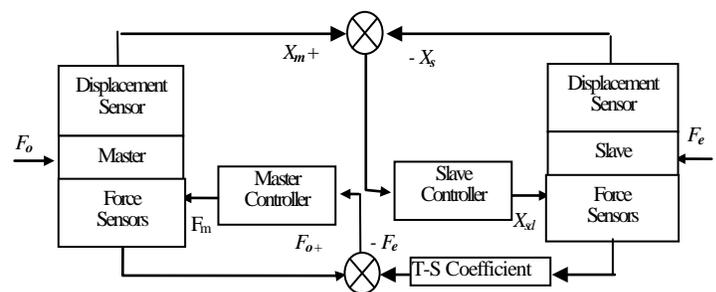


Fig.1 Structure of Improved force feedback tele-robot control system

The choice of the feedback coefficient, the usual practice is based on specific system feedback force range, select an appropriate ratio constant. However, this approach will force when feedback is small, the transparency of the system decreased significantly. The feedback coefficients should be expected of such a nature, force feedback when the feedback coefficient and a small number in order to enhance the sensitivity of force feedback. When the feedback force is large, the feedback factor should be smaller to ensure that force feedback can be put in the scope of the manpower in order to reduce the impact effects. In this paper, TS-type fuzzy model is constructed using non-linear changes in a continuous feedback coefficient to improve the force feedback control method. The improved control system schematic shown in Fig. 1, the main features of the control is the location of the Slave hand depend on the main and the secondly hand's position deviation between the control, the main force hand

feedback force by the product of F_e , K_{ef} and the operation of force bias control, the control law as follows:

$$F_m = K_f(F_o - K_{ef} * F_e), \quad X_{sd} = K_s(X_m - X_s)$$

Where:

- F_m --Drive Master Hand Vector;
- K_f --Main hand gain matrix;
- F_e --force vector from the secondly hand and the environment;
- F_o --The operator control force vector;
- X_{sd} --Expect position vector of the Slave hand;
- K_s --Displacement gain matrix of the Slave hand;
- X_m --Main hand displacement vector;
- X_s --Slave hand displacement vector;
- K_{ef} --Feedback coefficient.

3. The Structure of System

The tele-operation system with force tele-presence includes following components: the manipulator, electro-hydraulic servo drive system, displacement servo control system, visual tele-presence system, wireless communication system and force sensors, displacement sensors etc, shown in Fig.2.

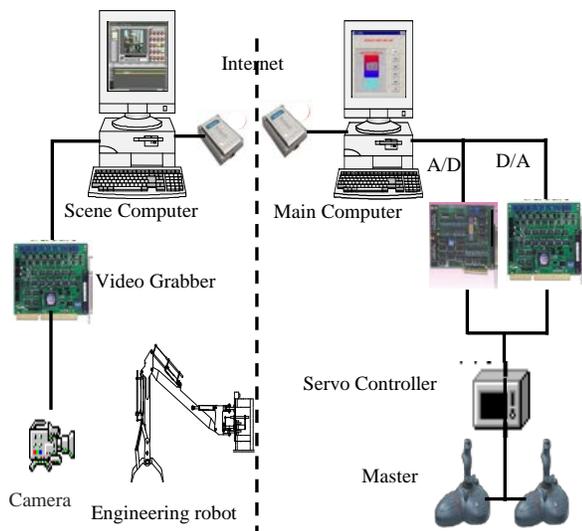


Fig. 2 Master-slave system for remote control

The figure shows that the system is constructed as a master-slave system and that both manipulators for the master and the slave consist of 4-DOF type actuators. Moreover, it is illustrated that a machine tool for grinding is implemented at the end-effector of the slave manipulator.

In a tele-operated master-slave system as shown in Fig. 1, the master has to play two roles, firstly as a reference input device to the slave, and secondly as a sense of force device. Here, the term “sense of force” means a function that allows the operator to feel a force that is fed back to him from the slave[7~9].

This research deals with a remote-control system applicable to the machining fields, such as grinding, polishing, assembling, and shaping. In machining works that require high speed, high power, and high rigidity in the operation, the attributes of hydraulic actuators make them suitable for these applications. In this study, we deal with a master-slave system composed of serial links by hydraulic cylinders. First, the serial links treated here are assumed to be of 1-DOF, and then of 4-DOF for general use, because we mainly are concerned with developing a new sense of force device.

At the first control stage, the remote control computer handclasps with the worksite one, and then the worksite computer reads the information of the joints’ displacement and velocity through the A/D continuously, and transmits all these information to the remote control computer to initialize the graphic robot and make the operator present the worksite robot’s state. Simultaneously, the worksite computer and the graphic computer receive the control instructions in the manner of event-driven. The graphic computer refreshes the virtual robot motion state on real time. The worksite computer explains the operator’s instructions into the motion angles of every joint by arithmetic, where the sampling and controlling interval is ten mms. The process is shown in Fig.3.

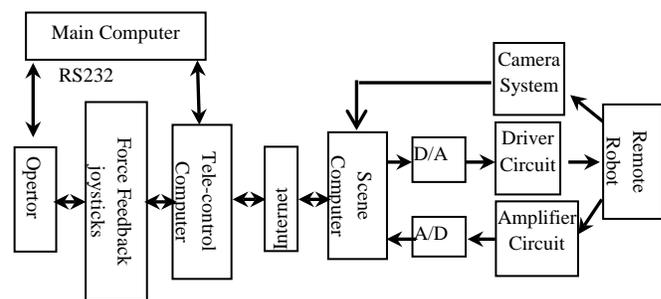


Fig.3 Remote Robot Control System Principle

When the operator operates the remote worksite robot facing to the simulation robot, the video information is needed to be watched on real time because the model errors between the graphic robot and the virtual environment are inevitable [5], and the worksite environment can also not be predicted. All these were completed by the equipments fixed on the remote robot

such as camera, video emitter, video receiver and so on[10,11].

Comparing with the tele-operation which is operated only by the video pictures transmitted from the worksite, the operation with high tele-presence prompt manner may enhance the work efficiency by 30%~50%. Simultaneously, it is not only favor for conquering the influence of time delay, but also can provide friendly graphical user interface. The operator can change video point and video angle of the conceals level forward feeds network [12~13]. It is non-linear from input to the output mapping, but it is linear from the conceals level space to the output space mapping, thus speeds up the study speed greatly and avoids the partial minimum problem.

4. Control algorithm realization

4.1 RBF nerve network model

The Radial Basis Function nerve network is proposed by J.Moody and C.Darken in the end of 1980s, it has three conceals level forward feeds network [14]. It is non-linear from input to the output mapping, but it is linear from the conceals level space to the output space mapping, thus speeds up the study speed greatly and avoids the partial minimum problem. RBF network architecture shows in Fig.4.

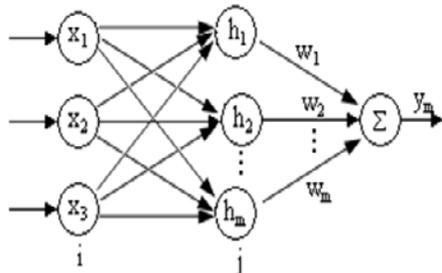


Fig.4 RBF Nerve Network Frame Chart

4.2 RBF nerve network PID control algorithm [15]

PID control to simple structure, robustness, good, able to adapt to the complex system control, etc., in the control engineering has been widely used [16,17]. But the parameters of conventional PID control system by setting a hard-line adjustment of the non-linear and non-deterministic system control result is not very satisfactory. To do this in cooperation with the Ziegler-Nichols method of digital simulation to determine the PID parameters of stable operation of the system K_p, K_i, K_d , after the initial value. Designed to use RBF (Radial Basis Function) neural network model for online identification system, and adjust

the PID parameters, the formation of RBF-PID controller to meet the remote operation of robot control system engineering nonlinear and uncertain requirements, its block diagram as follows in Fig.5.

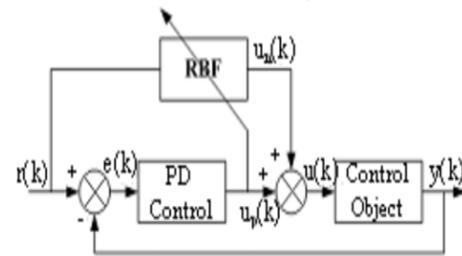


Fig.5 RBF Nerve Network PD control

RBF network is a three-layer feed forward network, from input to output mapping is nonlinear, while the hidden layer space to output space mapping is linear, thus speeding up the learning speed and avoid local minima problems [18~20]. This design network model has six input nodes, eight hidden layer nodes, three output nodes. According to the system model equation, to be ts as the sampling period, matching all the pole-zero conditions, to obtain the discrete model of the system:

$$y(k) = a_1 y(k-1) + a_2 y(k-2) + a_3 y(k-3) + a_4 u(k-1) + a_5 u(k-2) + a_6 u(k-3) \quad (1)$$

Where:

$y(k)$ —the output of the system of k time

$u(k)$ —the control input of K time

a_i —known constants of System model

$$X = [x_1, x_2, x_3, x_4, x_5, x_6]^T \quad (2)$$

Then the RBF network input vector:

Where:

$$x_i = y(k-i) \quad i=1,2,3$$

$$x_j = u(k-j+3) \quad j=4,5,6$$

Hidden layer nodes to take Gaussian kernel function:

$$h_j = \exp\left(-\frac{\|X - c_j\|^2}{2b_j^2}\right) \quad j=1,2,\dots,6 \quad (3)$$

Where: The first j nodes h_j center vector $c_j = [c_{j1}, c_{j2}, \dots, c_{j6}]^T$; the base width $b_j = [b_{j1}, b_{j2}, \dots, b_{j6}]^T$; knot vector $H = [h_1, h_2, \dots, h_6]^T$. Take the network weight vector $W = [w_1, w_2, \dots, w_6]^T$, using gradient descent method $c_{j\alpha}, b_j, w_j, h_j$ of the iterative algorithm is as follows:

$$y_m(k) = w_1 h_1 + w_2 h_2 + \dots + w_6 h_6 \quad (4)$$

$$w_j(k) = w_j(k-1) + \eta \left(y(k) - y_m(k) h_j + \alpha (w_j(k-1) - w_j(k-2)) \right) \quad (5)$$

$$b_j(k) = b_j(k-1) + \alpha(b_j(k-1) - b_j(k-2)) + \eta \Delta b_j \quad (6)$$

$$c_{ji}(k) = c_{ji}(k-1) + \alpha(c_{ji}(k-1) - c_{ji}(k-2)) + \eta \Delta c_{ji} \quad (7)$$

Which take learning rate $\eta=0.2$, Momentum factor $\alpha=0.05$.

$$\frac{\partial y(k)}{\partial u(k)} = \frac{\partial y_m(k)}{\partial u(k)} = \sum_{j=1}^m w_j h_j \frac{c_{ij} - u(k)}{b_j^2} \quad (8)$$

Incremental PID coefficient adjustment method is as follows:

$$E(k) = R(k) - y(k) \quad (9)$$

Where: $R(k)$ —The system reference input.

$E(k)$ —System error.

$$\Delta k_p = -\eta \frac{\partial J}{\partial k_p} = \eta E(k) \frac{\partial y(k)}{\partial u(k)} (E(k) - E(k-1)) \quad (10)$$

$$\Delta k_i = -\eta \frac{\partial J}{\partial k_i} = \eta E(k) \frac{\partial y(k)}{\partial u(k)} \quad (11)$$

$$\Delta k_d = -\eta \frac{\partial J}{\partial k_d} = \eta E(k) \frac{\partial y(k)}{\partial u(k)} \left(\frac{E(k) - 2E(k-1)}{+E(k-2)} \right) \quad (12)$$

$$u(k) = u(k-1) + K_p(E(k) - E(k-1)) + K_i E(k) + K_d(E(k) - 2E(k-1) + E(k-2)) \quad (13)$$

5. Experiment results

To realize a tele-operated manipulation system as shown in Fig. 1, it is necessary to constitute a master-slave system, in which the master and the slave correspond, respectively, to a sense of force and an actuating manipulator. In this section we therefore discuss a master-slave hydraulic system equipped with the new sense of force proposed.

5.1 System Constitution

In Fig.6, a schematic diagram of the experimental apparatus for the present study is shown. The total system consists of a master system and a slave system. The operator's force F_{op} , detected by a force sensor, is sent to the computer in order to actuate a master-side piston. In the slave system, a spring of stiffness k is attached at a frame of apparatus for simulating a load-force of operation. To detect the load-force, a force sensor is set at the inertial load through a plate spring. Two displacements of pistons in master and slave x_m , x_s , and two forces $F_{op} = F_m$, F_s are detected by each sensor and then sent to the computer. Subsequently, two control inputs u_m and u_s for actuating the master and the slave are calculated in the computer,

according to a bilateral algorithm. For an algorithm of each controller for the master and slave, a proportional control algorithm was adopted. The sampling time was chosen to be 1 ms. In the experiment, two kinds of load, that is tires and hardwood, were tested. With respect to servo-valves and cylinders for constructing two servo-systems in the master and the slave, different types were adopted intentionally between the two systems. Namely, the master-slave system was tested in the experiment for a system with rather different dynamic characteristics between the master and the slave.

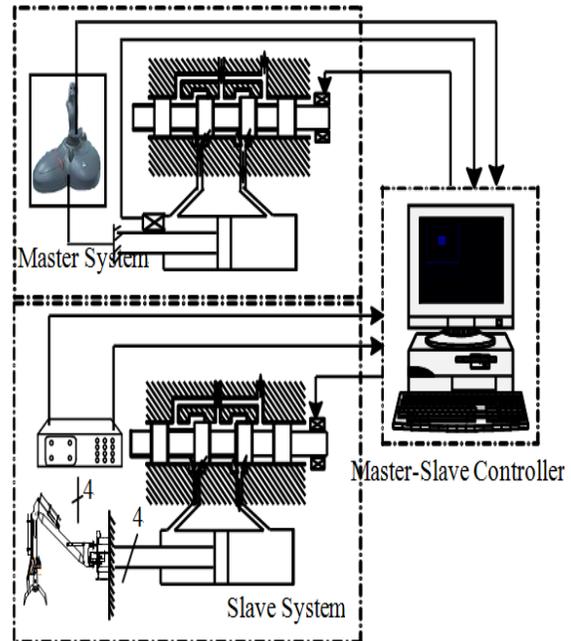


Fig. 6 Diagram of experimental apparatus

It is adopted that a bilateral control methodology for controlling the master-slave system. Concerning system constitutions for bilateral control, the following two types are well known as representative ones: (a) Force reflecting servo type and (b) Parallel control type.

5.2 Experimental Results

In the master-slave system shown in Fig.7, two types of bilateral controls are adopted, that is, a force reflecting servo type and an improved parallel control method. By comparing the force functions between two types of systems, we investigate experimentally the applicability of the proposed system. In the experiment, time responses of two forces F_m and F_s were measured together with those of two displacements X_m and X_s .

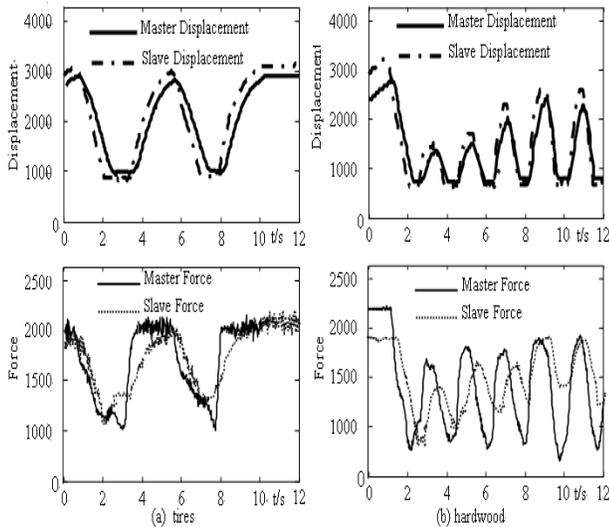


Fig.7 Experimental results of force reflecting servo type

First, response curves for the force reflecting servo system are shown in Figs.7(a) and (b). These figures correspond, respectively, to the results for the tires and the hardwood. Observing Fig. 7(a), it is shown that the slave force F_s is detected almost at the instant that the slave touches the tires. Subsequently, the force F_s is controlled in good agreement with the master force F_m is shown in the figure. In this experiment, the operator was able to feel a softness of tires through the sensing function of the sense of force. On the other hand, Fig.7(b) shows that the response curve of F_s is accompanied by a tendency toward vibration. The vibration appears from the instant that the slave touches at the tires. In addition, the tendency of such a vibration affects the waveforms of displacements X_m and X_s . In this experiment, it was difficult to control the system stably. Secondly, the same kinds of results as seen in Fig. 7 are shown in Figs. 8 (a) and (b) as a result of the parallel control. Through comparing Fig.8(a) and Fig. 7(a), it is shown that both results coincide well with each other. The operator in this experiment was able to feel a softness of tires as in the previous experiment in Fig.7(a). Furthermore, the result for the hardwood from Fig.8(b) is improved distinctly compared with the result in Fig.7(b). The system was kept stable in this experiment under various system conditions. As a result, the operator was able to feel a hardness of wood. Correspondingly, it is observed in Fig.8(b) that the amount of piston displacement is smaller than in Fig.8(a), in spite of the fact that a larger force than that in (a) is given to the system.

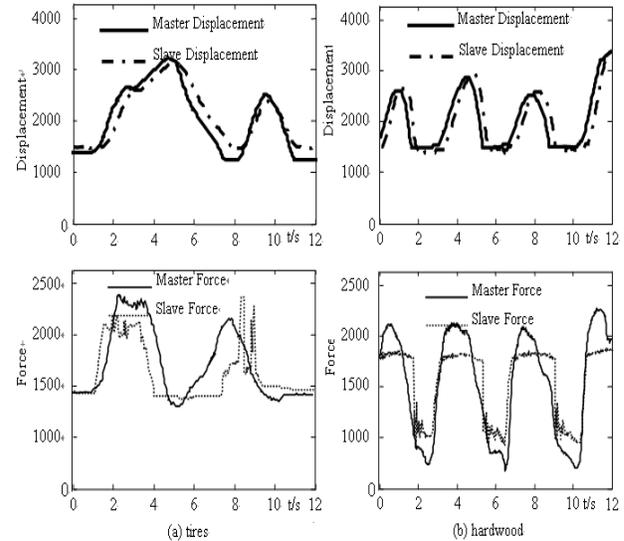


Fig.8 Experimental results of parallel control method

6. Conclusions

In view of the novel force feedback bilateral servo control system, it was proposed that one kind of RBF nerve network tuning PD on-line from study, adaptive control strategy, which can approach willfully the continuous function characteristic using the RBF nerve network by the free precision, through optimizing two parameters of PD by RBF nerve network, it can improve dynamic characteristic of master-slave control system. Through simulation and experiments, firstly, it can be theoretically proved that this control algorithm of novel force sense bilateral servo system is practical and feasible; next, this algorithm can realize master-slave position tracking and let the operator feel "the force sense" well from feedback, thus improves the human and the environment interaction characteristic and enhances the working efficiency. Moreover, this control arithmetic has taken on control briefness, constringency rate rapidness, real-time well, strong robustness, self-adapted and the rapidity.

References

- [1] S.Munir, W.j.Book, "Internet Based Tele-operation using wave variables with prediction", in proceedings of IEEE/ASME International conference on advanced intelligent mechatronics, 2001, Vol. 1, pp. 43-50.
- [2] K.Hidetoshi, H.Yamada,T.Muto,"Mater-Slave Control for a Tele-Operation System of Construction Robot", Transactions of the Japan Fluid Power System Society, 2003, Vol. 34,No. 2, pp. 27-33.
- [3] M.D.Gong, D.X.Zhao, T.Ni etal., "Design of an Isomeric Slave Arm for Engineering Robot", Construction Machinery and Equipment, 2003, No. 12, pp. 1-3.

- [4] S. Kudomi, H. Yamada, and T. Muto, "Development of a Hydraulic Parallel Link Force Display Improvement of Manipulability Using a Disturbance Observer and its Application to a Master-slave System", *Journal of Robotics and Mechatronics*, 2003, Vol. 15, No. 4, pp. 391-397.
- [5] X.X.Tang, H. Yamada, D.X. Zhao, T. Ni, "Haptic Interaction in Teleoperation Control System of Construction Robot Based on Virtual Reality", in *Proceedings of the 2009 IEEE International Conference on Mechatronics and Automation*, 2009, pp. 78-83.
- [6] Y. Ye, Y.J. Pan, Y. Gupta, "Time domain passivity control of teleoperation systems with random asymmetric time delays", In *Proceedings of the 48th IEEE Conf. on Decision and Control*, 2009, pp. 7533-7538.
- [7] J. Ware, Y.J. Pan, "Realisation of a bilaterally teleoperated robotic vehicle platform with passivity control", *IET Control Theory & Applications*, 2011, vol. 5, no. 8, pp. 952-962.
- [8] E. Slawinski, V.A. Mut, P. Fiorini, L.R. Salinas, "Quantitative Absolute Transparency for Bilateral Teleoperation of Mobile Robots," *Systems, Man and Cybernetics, Part A: Systems and Humans*, *IEEE Transactions on*, 2012, vol. 42, no. 2, pp. 430-442.
- [9] T. M. Lam, H. W. Boschloo, M. Mulder, and M. M. Van Paassen, "Artificial force field for haptic feedback in UAV teleoperation", *IEEE Trans. Syst., Man, Cybern. A, Syst., Humans*, 2009, Vol. 39, No. 6, pp. 1316-1330.
- [10] E. Slawiński and V. A. Mut, "Control scheme including prediction and augmented reality for tele-operation of mobile robots", *Robotica*, 2010, Vol. 28, No. 1, pp. 11-22.
- [11] Y. Wagatsuma, Y. Toda, N. Kubota, "Formation behavior of multiple robots based on tele-operation", In *Proceedings of 2011 IEEE International Conference on Fuzzy Systems*, 2011, pp. 713-720, 27-30.
- [12] C. Ishii, H. Mikami, T. Nakakuki and T. Hashimoto, "Bilateral Control for Remote Controlled Robotic Forceps System with Time Varying Delay", In *Proceedings of 2011 4th International Conference on Human System Interactions*, 2011, pp. 330-335.
- [13] C. Ishii, K. Kobayashi, Y. Kamei and Y. Nishitani, "Robotic Forceps Manipulator with a Novel Bending Mechanism", *IEEE/ASME Transactions on Mechatronics*, 2010, Vol. 15, No. 5, pp. 671-684.
- [14] S.C. Cramer, "Brain repair after stroke", *New England Journal of Medicine*, 2010, Vol. 362, pp. 1784-1787.
- [15] L. Dipietro, H.I. Krebs, S.E. Fasoli, B.T. Volpe, N. Hogan, "Submovement changes characterize generalization of motor recovery after stroke", *Cortex*, 2009, Vol. 45, No. 3, pp. 318-324.
- [16] P.W. Duncan, R. Zorowitz, B. Bates, J.Y. Choi et al., "Management of adult stroke rehabilitation care: a clinical practice guideline". *Stroke*, 2005, Vol. 36, No. 9, pp. 100-143.
- [17] Y. Hsieh, C. Wu, W. Liao, K. Lin, K. Wu et al., "Effects of treatment intensity in upper limb robot-assisted therapy for chronic stroke: a pilot randomized controlled trial". *Neurorehabil Neural Repair*, 2011, Vol. 25, No. 6, pp. 503-511.
- [18] D.E. Nathan, M.J. Johnson, J.M. McGuire, "Design and validation of a low-cost assistive glove for assessment and therapy of the hand during ADL-focused robotic stroke therapy", *J Rehabil Res Dev*, 2009, Vol. 46, No. 5, pp. 587-602.
- [19] W.S. McCombe, W. Liu, J. Whitall, "Temporal and spatial control following bilateral versus unilateral training", *Human Movement Science*, 2008, Vol. 27, No. 5, pp. 749-758.
- [20] A.C. Lo, P. Guarino, L.G. Richards, et al., "Robot-Assisted Therapy for Long-Term Upper-Limb Impairment after Stroke", *New England Journal of Medicine*, 2010, Vol. 362, pp. 1772-1783.

Guang Wen received a B.E. degree from Sichuan University of science and engineering, Zigong, China, in 1997 and a Master Degree in Mechanical and Electronic Engineering from Jilin University, Changchun, China, in 2008. He is now a professor at Panzhihua University. His research interests cover Tele-operation robotics, Numerical Control.